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A 31 T split-pair pulsed magnet for single crystal x-ray diffraction at low temperature

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We have developed a pulsed magnet system with panoramic access for synchrotron x-ray diffraction in magnetic fields up to 31 T and at low temperature down to 1.5 K. The apparatus consists of a split-pair magnet, a liquid nitrogen bath to cool the pulsed coil, and a helium cryostat allowing sample temperatures from 1.5 up to 250 K. Using a 1.15 MJ mobile generator, magnetic field pulses of 60 ms length were generated in the magnet, with a rise time of 16.5 ms and a repetition rate of 2 pulses/h at 31 T. The setup was validated for single crystal diffraction on the ESRF beamline ID06. © 2014 AIP Publishing LLC. [<http://dx.doi.org/10.1063/1.4878915>]

I. INTRODUCTION

Of all x-ray techniques, single crystal diffraction with a monochromatic beam offers by far the highest resolution, the strongest absolute signal, and the best signal to noise ratio. It is therefore the method of choice for the examination of small crystallographic changes (such as magneto-elastic effects), and for weak signals (such as magnetic scattering or scattering of orbital order). Furthermore, in many cases the magnetic field induced effects are anisotropic and require the application of the field along a specific crystallographic axis, which can only be realized with single crystal samples, and not polycrystalline ones. An optical access over a wide angular range is often required in order to enable measurements at high scattering angles.

With this specific aim, the simplest way to obtain a magnet with large optical access in the mid plane perpendicular to the magnetic field is to use two coils, series connected and axially aligned, with a gap between them. In this arrangement, commonly called split-pair magnet, the vertical axial bore is used to insert the sample cryostat, and the horizontal mid plane gap is used for x-ray access. Even though they constitute great mechanical design challenges to avoid the collapsing of the two coils, several pulsed magnets of split-pair type¹⁻⁵ have been developed over the last 10 years to meet the requirements for combining x-ray diffraction with high pulsed magnetic field. Solenoid magnets were also realized⁶⁻⁸ as they can offer, with the same energy, larger pulsed magnetic fields at the center of the coil, however at the price of a reduced opening angle ($\pm 13^\circ$,⁶ $\pm 31^\circ$,⁷ and $\sim 23.6^\circ$ ⁸).

Unlike x-ray diffraction techniques such as white beam Laue diffraction or powder diffraction, single crystal diffraction requires precise alignment of the sample and is therefore sensitive to vibrations that might be introduced by

electromagnetic forces induced by the field pulse. The magnet and diffractometer set-up must therefore be optimized to reduce vibrations. This is not only the case for split-pair type magnets, but also for other magnet designs.⁸ Unfortunately, few publications have shown the difficulties and the efforts required to reduce the pulse induced vibrations⁸ allowing to make x-ray single crystal diffraction compatible with pulsed magnetic field.

Here, a new pulsed field set-up, including a 31 T split-pair magnet and a sample cryostat, both specifically designed and optimized for single crystal measurements on a synchrotron x-ray beamline, is presented. Compared to recently developed split-coil magnets of other groups,¹⁻⁵ our split-coil offers a much increased field pulse duration (60 ms compared to ~ 1 ms^{1,4,5} to 27 ms^{2,3}), a wider angular range of $\pm 180^\circ$ in 2θ and a longer rise time of 16.5 ms. The latter feature is an advantage leading to less sample heating induced by eddy currents⁹ and also compensates for the shorter cool-down time between field pulses required by the aforementioned devices (~ 10 to 20 min^{2,3,5} compared to half an hour for our split-coil). In addition, our device offers the possibility to invert the magnetic field polarization and to change the sample temperature over a wide range (from 1.5 to 250 K) while optimally cooling the coil. Particular efforts have been carried out to quantify the vibrations of this new set-up. Several technical changes have been made on the pulsed magnet and cryogenic assembly by the LNCMI-Toulouse (LNCMI-T) and on the beamline at the ESRF-Grenoble, to minimize the vibrations and their propagation.

After a detailed description of the different parts of the system we present its main features as regards of field, temperature, angular resolution and stability, illustrated by first results obtained on a Fe_{1.1}Te single crystal.

II. PULSED FIELD DEVICE AND CRYOGENICS

A. The split-pair magnet: Design and construction

The split-coil magnet described here was designed and built at the LNCMI-T. It is composed of two coils consisting of 36 layers of 13 turns. The wire choice was the result of a trade-off between low resistivity to reduce coil heating and high ultimate tensile stress (UTS) to resist to magnetic pressure. A copper conductor, internally reinforced by niobium titanium filaments and insulated with kapton, was used. Its main features are reported in Table I.

The usable space for sample and cryogenics is determined by the magnet bore diameter and the gap between the two coils. Stainless steel spacers were inserted between both magnets to withstand the pressure (~ 200 MPa) resulting from attraction induced by Lorentz forces on the two coils. These spacers were designed with 16° open sectors for x-ray beam access alternating with 14° closed sectors (see Fig. 1). A thin layer of Teflon and 2 mm of glass fiber epoxy composite (FR4/G10) were added between the coils and the spacers to increase electrical insulation and internal mechanical reinforcement.

With an inner diameter of 22 mm, an outer diameter of 200 mm, a height of 50 mm per coil, and a gap of 20 mm, the total height of the split-pair magnet is 120 mm and the resulting inductance $L = 35$ mH. At the center of the magnet, the vertical length available for the sample is of ± 2.5 mm and the vertical angular opening of each open sectors is of $\pm 2.5^\circ$ (see Fig. 2).

This split-pair magnet was designed to generate a maximum field of 30 T at the sample position. This design goal was achieved as the final coil reached a field of 31 T in user operation.

B. Cryogenic environment description

The cryogenic system consists of a liquid nitrogen (LN2) bath cryostat that houses the coils, and a separate liquid ^4He cryostat for the sample.

1. LN2 bath cryostat

The split-pair magnet was integrated into a custom designed nitrogen cryostat equipped with 12 x-ray transparent, vacuum tight Kapton windows (foils of $120\ \mu\text{m}$ thickness). The latter are distributed around the Dewar (Fig. 1), matching the 16° optical access sectors in the spacers between the

TABLE I. Main mechanical and electrical properties of the wire conductor. The copper wire was reinforced by 630 NbTi filaments of around $80\ \mu\text{m}$ diameter. The volume fraction of the NbTi determined from the number of filaments and their average diameter is around 56.6%.

Cross section	$5.77\ \text{mm}^2$
Thickness \times width	$2\ \text{mm} \times 3.15\ \text{mm}$
Ultimate tensile stress	$\text{UTS}_{77\text{K}} \sim 1\ \text{GPa}$
Resistivity	$\rho_{77\text{K}} \sim 0.35\ \mu\Omega\ \text{cm}$ $\rho_{300\text{K}} \sim 2.9\ \mu\Omega\ \text{cm}$

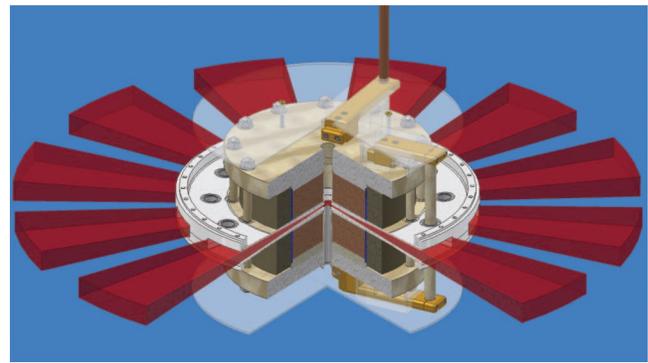


FIG. 1. Three-dimensional view of the split-pair magnet. The optical access for x-ray beam in the mid-plane is highlighted by the red color.

magnets. The internal vessel of this cryostat is divided in two parts (the lower and upper baths), each containing a coil (Fig. 3). A stepped tube, intended to house the ^4He insert, passes through the bore of the split-coil. Connection and continuity between the lower and upper baths are ensured by 12 stainless steel tubes traversing the spacers. This configuration allows the use of a common vacuum for the nitrogen cryostat, the helium insert, and the x-ray beam path.

2. ^4He insert cryostat

The coil/LN2 cryostat assembly hosts a top loading ^4He cryostat allowing measurements in the temperature range 1.5–250 K.

As shown in Figures 3 and 4, it is a double baths type cryostat (the main bath and the 1.5 K bath with its extension), equipped with a 2.5 K heat exchanger and a heater. It also includes a circulation loop which enables to work in closed cycled mode, thus increasing the operating autonomy at low temperatures.

The main bath (tank 1) is a 3 l liquid helium vessel equipped with a liquid helium level sensor (with gauge unit model HLG210 from Cryogenic) so that it can be automatically refilled. It is connected with the 1.5 K bath (tank 2, 0.4 l) via a tube of 2 mm inner diameter equipped with a cold valve. When open, the valve allows refilling of tank 2 with liquid ^4He from the main bath while, when closed, tank 1 can be refilled with almost no effect on the temperature of tank 2. The design of a double baths type cryostat, as described here, enables to use the upper bath as a reserve of liquid ^4He whereas the lower bath will be pumped to reach temperatures as low as

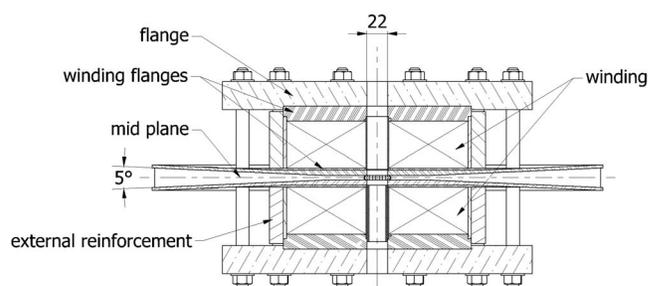


FIG. 2. Cross-section of the split-pair magnet.

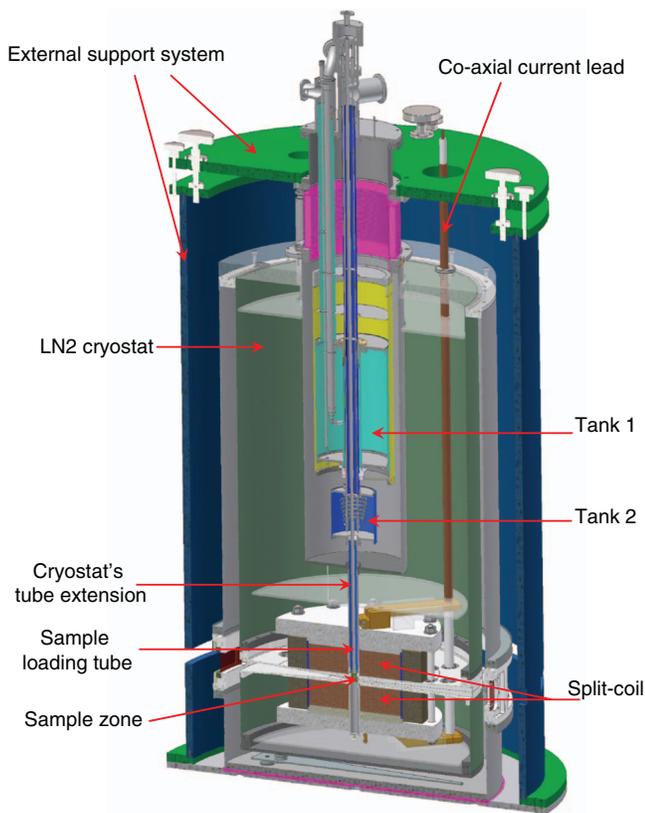


FIG. 3. Three-dimensional schematic view of the split-pair magnet and cryogenic environment.

1.5 K. Thanks to the small volume of the lower bath, the cooling down to 1.5 K is very quick and is made at low expenses of liquid ^4He .

The cryostat also includes a 2.5 K heat exchanger (Fig. 4) pumped by an independent pumping line. This exchanger is continuously supplied with liquid helium coming from the tank 1 and includes in its lower part a Joule Thomson (J-T) impedance (capillary of 10 cm length and 0.15 mm inner diameter) allowing the expansion of the helium gas and, therefore, the cooling of the vapors in the inner part of the exchanger down to 2.5 K. In closed cycle mode, the He flow is injected through a long capillary, the capillary for close-loop circulation (see Fig. 4) (stainless steel tube of 1.2 m length and 1 mm inner diameter). The latter is wound inside the exhaust line of the tank 1, traversing the tank 1 and the exchanger. Thus, the circulated gas is pre-cooled before entering the upper part of the tank 2. The flow is then distributed via two needle valves in two different lines. The first valve allows to regulate the temperature between 4 and 250 K, the line being wound around the joule heater's support located in the lower part of the cryostat's tube extension. The second valve allows to reach temperatures as low as 1.5 K, this line being extended by a long and thin capillary (1 m length and 0.5 mm inner diameter) twisted inside the cryostat's tube extension and ending with a final impedance (capillary of 5 cm length and 0.15 mm inner diameter).

To allow a quick and safe loading of the sample, the cryostat is completed with a sample loading system which separates the sample space from the bath containing liquid

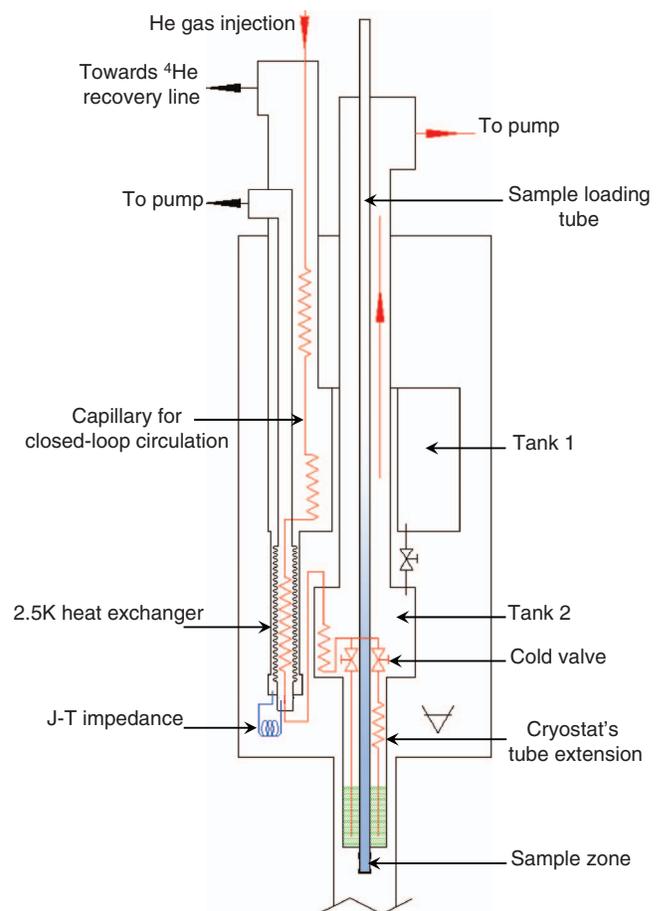


FIG. 4. Scheme of the ^4He insert cryostat.

^4He . It consists of a top-loading tube (of 7.6 mm inner diameter and 0.2 mm thick) going through the whole length of the insert (from the top at room temperature down to the vicinity of the magnetic field center), equipped with a vacuum lock arrangement. The sample loading tube ends with the sample zone, located at the center of the magnetic field. It consists of a capsule of 800 μm thick Torlon, a polymer fairly transparent to x-ray, glued with Stycast 2850 FT. A brass foil tube, radially drilled and thermally anchored to the cryostat tube extension, surrounds the capsule and is covered with several layers of super insulation to screen against the thermal radiation from the Kapton windows at room temperature. The sample zone and the loading tube were designed to be easily evacuated, then loaded with a few cm^3 of ^4He exchange gas at room temperature and pressure. In operation the external surface of the loading tube is in direct contact with the liquid ^4He of the cryostat tube extension while its internal surface is in contact with the exchange gas. The sample is thus cooled down by exchange gas to the bath temperature.

To mechanically decouple the ^4He insert from the magnet and LN2 cryostat, and to allow fine adjustment of the ^4He cryostat's tube extension inside the vacuum enclosure, an additional external support system (Fig. 3) was built in order to avoid mechanical and thermal contact.

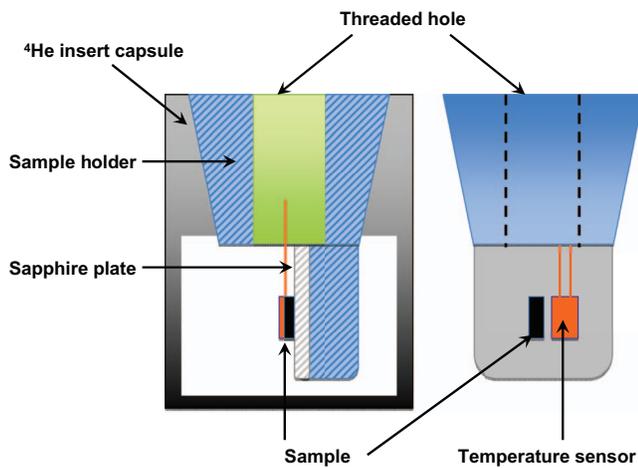


FIG. 5. Schematic views of the sample holder: (left) cross section of the sample holder inserted inside the capsule of the ^4He insert, (right) front view. The temperature sensor is glued close to the sample and connected to a Lakeshore temperature controller via the measurement stick screwed into the threaded hole. ^4He exchange gas flows around the sample thanks to holes drilled in the measurement stick and sample holder (not shown here).

Finally, a sample handling system has been designed specifically to prevent sample motion (rotation and/or translation of sample holder) induced by field pulses. It consists of the sample holder coupled with the capsule located at the bottom of the ^4He insert. Both parts are made in Torlon, thus avoiding eddy currents in the sample holder. The upper parts of both elements have a conical shape (see Fig. 5) allowing to physically lock the sample holder inside the ^4He cryostat after alignment of the sample in Bragg condition. The stability of the sample orientation is thus ensured over time. The sample handling system is complemented with a measurement stick which is equipped with a calibrated temperature sensor (Cernox), a pick-up coil, and a heating resistance. To improve thermal conductivity, a thin sapphire plate (thickness $\approx 400\ \mu\text{m}$) is glued to the sample holder. Both sample and temperature sensor are then stuck on the plate with GE varnish.

All the cryogenic environments have been custom designed and built at the LNCMI-T.

C. Generator

The split-pair magnet was used with a 24 kV, 1.15 MJ transportable pulsed field generator developed by the LNCMI-T. This generator consists of two identical storage units and one control unit. Each storage unit contains eight high energy density capacitors of $250\ \mu\text{F}$ each, resulting in a total capacitance of 4 mF, two crowbar resistors ($R_{\text{crowbar}}(\text{total}) = 2\ \Omega$), and two inductive current limiters ($L(\text{total}) = 1.845\ \text{mH}$). The control unit houses the charger, thyristor stack, dump resistors, and the current and voltage monitors. This unit is also equipped with high-voltage, high-current pneumatically driven commutators to give the possibility to work with two polarities. Commutation and charging take only a few minutes and is controlled completely by a computer integrated in the central control unit. The energy of the capacitor bank is released into the coil through an optically triggered thyristor switch. The bank is protected from

failure in case of a short in one capacitor. To avoid an electrical dump of all the other capacitors into the defective one, they are all equipped with industrial high voltage fuses.

The three subunits are mounted in individual steel frames so that they can be transported using a fork lift or an overhead crane. Each storage module weighs approximately 2000 kg and has dimensions ($h \times d \times w$) $2.00 \times 1.60 \times 1.20\ \text{m}^3$. The control unit is slightly smaller ($1.50 \times 1.60 \times 1.20\ \text{m}^3$) and weighs only 800 kg. The connections between the three subunits are made on external patch panels and do not require opening of the units' enclosures. The generator can thus be safely installed by users with minimal training. For our synchrotron experiments, the generator, located outside the experimental hutch, was linked to the personal safety system (PSS) of the radiation hutch such that it could be charged only after the hutch had been searched and interlocked.

III. COMMISSIONING

A. Coil operation

The coil parameters as measured during coil testing were: a resistance value $R_{\text{coil}} = 192\ \text{m}\Omega$ and $1650\ \text{m}\Omega$ at 77 and 300 K, respectively, an inductance $L = 35\ \text{mH}$ and a field factor of $169.2\ \text{A/T}$.

Maximum magnetic field of 31 T was achieved at the center of the split-pair magnet for a charging voltage of $V = 18\ \text{kV}$. The pulse duration was of 60 ms with a rise time of 16.5 ms, as shown in Figure 6. With more than 4.5 ms above 98% of the maximum field value, this pulse is relatively long compared to the other pulsed field devices developed for x-ray and neutron scattering experiments.^{1-5,8,10,11} In addition, the magnetic field produced at the center of the magnet shows less than 1% of variation over $\pm 3\ \text{mm}$ along the bore of the magnet and less than 0.5% radially (over a radius $R = 3\ \text{mm}$), which means a very high homogeneity over typical size of single crystals probed by x-ray (i.e., from hundreds of micrometers to one or two millimeters). The energy stored into the coil at maximum field value is relatively high ($\sim 480\ \text{kJ}$) and at the end of the pulse its electrical resistance shows an increase of about $250\ \text{m}\Omega$ equivalent to a coil heating of 40 K. Around half an hour is then required between two pulses at 31 T to return to the coil operating temperature of 90 K.

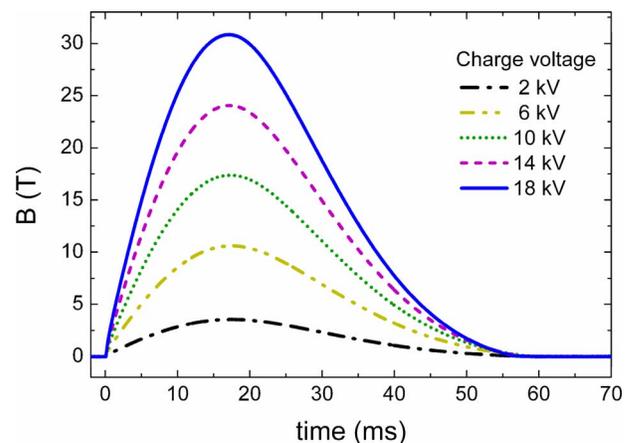


FIG. 6. Pulse field shape as measured at different charge voltages.

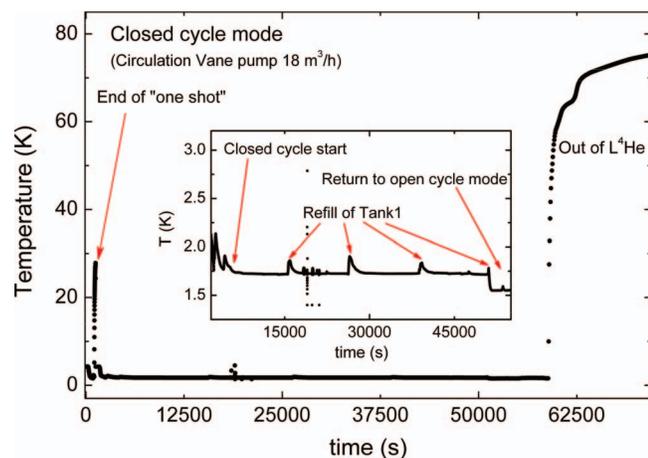


FIG. 7. Monitoring of temperature when the ^4He insert cryostat is used in closed cycle mode. The working temperature was measured with a CX-1050-SD Cernox sensor, calibrated down to 1.4 K. To obtain 1.5 K, the Edwards E2M18 Hermetic circulation pump was replaced by a E2M40 pump.

B. Low temperature measurements

The cryogenic performances have been tested successfully in open cycle and closed cycle mode. In open cycle mode tank 2 is filled with liquid ^4He at 4.2 K by opening the cold valve between tanks 1 and 2. The cold valve is then closed, and by pumping on tank 2 a sample temperature of 1.5 K can be obtained within a few minutes. This temperature can be maintained for around 3 h before tank 2 has to be refilled. In this mode, the cooling capacity measured at sample site, when a rotary vane pump (Edwards E2M18) is used, is 36 mW at 1.6 K.

In closed cycle mode, a continuous flow of cold He gas arrives close to the sample zone through the circulation loop capillary whereas only the bottom part of tank 2 (tube extension) is filled with a few cm^3 of liquid ^4He . By pumping on tank 2 with a E2M40 rotary vane pump, a base temperature of 1.5 K (1.7 K when using a E2M18 pump, as shown in Fig. 7) is reached within less than 20 min and can be maintained for more than 13 h provided that tank 1 is refilled periodically. To avoid an increase in temperature when the sample is exposed to x-ray, absorber foils are added before the sample in the incident beam path, so that only 10%–20% (i.e., $\sim 10^{12}$ photons/s at 11 keV) of the incident flux are kept. In addition, a fast x-ray shutter (LS200 Laser shutter from NM Laser products, Inc. (San Jose, CA, USA)) is used to expose the sample during very short time (100 ms per magnetic field pulse).

IV. HIGH RESOLUTION X-RAY SINGLE CRYSTAL DIFFRACTION AND PULSED MAGNETIC FIELD

Commissioning tests of the split-pair magnet were performed on the undulator beamline ID06 (ESRF, Grenoble, France).

The source device was a cryogenically cooled permanent magnet undulator (CPMU)¹² with 18 mm period and 6 mm minimum gap, such that the first harmonic could be tuned from 10.5 keV to 19.0 keV. A liquid nitrogen cooled Si (111) double crystal monochromator selected photons with a

relative band width of $\approx 1.4 \times 10^{-4}$. The maximum achievable photon flux was about 2×10^{13} photons/s at 11 keV.

The cryostat and magnet assembly was installed in the experimental hutch 2 (EH2) on a high-load six circle diffractometer identical to that of ID20.¹³ The generator was installed in an enclosure outside of the experimental hutch, and connected to the magnet via a coaxial cable. A pneumatically operated switch disconnected the generator from the magnet when the hutch was not interlocked, i.e., when access to the hutch was allowed.

A. Characterization of vibrations and angular stability

The tests were first carried out on silicon single crystals to estimate the vibration amplitude of the complete device. The diffracted intensities were measured with a silicon photodiode mounted on the detector arm of the diffractometer and recorded (along with generator voltage and current, and the voltage on a pick-up coil on the sample stick) during the field pulses on a digital data recorder (HIOKI Memory HiCorder model 8860). Motorized slits upstream of the photodiode detector at 70 cm from the sample position were used to adjust the longitudinal (2θ) resolution. Due to the very narrow rocking curve width of the silicon crystal and the low divergence of the incident x-ray beam this configuration is extremely sensitive to rotations of the sample during the field pulse.

One main source of vibrations identified on the beamline was eddy currents propagating in the aluminium parts of the diffractometer. To increase the distance from the field center to those parts and suppress the repulsive forces generated by induced currents, several aluminium parts such as the goniometer top plate and rotation stages (χ and φ stages) of the diffractometer were removed and replaced by fiber glass spacers (FR4/G10). The remaining aluminium parts were thus located at more than 49 cm from the center of the magnet. Induced eddy currents and corresponding forces were sufficiently weak to not disturb the measurement anymore.

As an example, the evolution of the normalized intensity of a Si (800) Bragg reflection ($\text{FWHM}(\theta) \approx 0.004^\circ$) is shown in Figure 8 (left) as a function of time for different amplitudes of field pulses: 14, 21, and 31 T. The intensity begins to oscillate 9 ms after the magnetic field pulse was triggered. However, the variation of intensity does not exceed 17% during the first half of the pulse (i.e., up to 28 ms after the beginning of the pulse). Then, between 28 and 60 ms, the amplitude of the oscillation increases, with the intensity even going through zero for the 31 T pulse. The orientation of the sample is nevertheless maintained since the intensity is recovered with no more oscillation 1 s after the pulse (not shown).

By measuring the change of intensity at slightly lower or higher sample angles (θ) than the Bragg position, it was possible to ascribe the loss of intensity to sample rotation. The latter was easily calculated as a function of time based on the full width at half maximum of the reflection and pseudo-Voigt like shape of Bragg peaks. The result is displayed in Figure 8 (right). These curves show that sample rotation is always lower than $\pm 0.001^\circ$ during the first half of the pulse and does not exceed $\pm 0.0005^\circ$ at maximum field, well below the mosaicity of most single crystal samples of interest for high-field

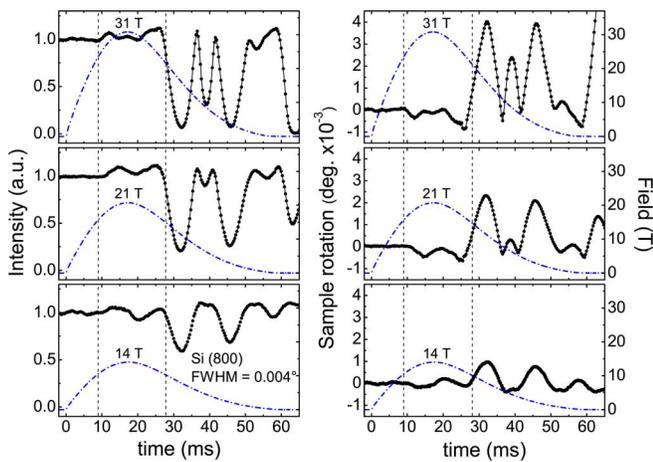


FIG. 8. (Left) Evolution of normalized intensity of a Si (800) Bragg reflection ($\text{FWHM}(\theta) \approx 0.004^\circ$) as a function of time for different magnetic field pulses. The pulsed field traces are represented by the dashed-dotted lines. (Right) Corresponding sample rotation as a function of time. Incident x-ray energy was $E = 31 \text{ keV}$ ($\lambda = 0.3995 \text{ \AA}$).

studies (e.g., $>0.05^\circ$ for typical intermetallic compounds). In the second half of the pulse, the rotation is as high as 0.004° for the shot at maximum field value.

This means that our experimental setup is not suitable for studying intensity changes over the entire field pulse for very high quality samples with mosaicity below 0.005° . One should note, however, that the usable pulse length (defined here as the pulse duration for which the sample rotations induced by vibrations are lower than $\pm 0.001^\circ$), i.e., the first 28 ms of the pulse, is at least five times longer than the one provided by the other pulsed field devices dedicated to x-ray single crystal diffraction experiments.^{2,3,5,8} As a matter of fact, they typically offer only ~ 1 to 5 ms per field pulse even when the pulse length is of 27 ms, the exposure time being indeed synchronized with the peak value of the pulse.^{2,3} The long duration of our pulse is then an advantage to measure metallic samples and hysteretic behaviors, but also weak signals such as super-lattice peaks since longer exposure times can be provided.

Other efforts have been carried out to further suppress or reduce vibrations, but they yielded no significant improvement, e.g., decoupling the coil cryostat from the diffractometer and sample cryostat by means of viscoelastic absorbers, and increasing the stiffness of the diffractometer by means of external reinforcements.

While simple, cheap, and easy to use, a point detector such as a photodiode requires at least one magnetic field pulse per scattering angle, and is thus not exactly very efficient for studies of magnetic field induced crystallographic phase transitions. On the other hand, a fast 2D detector can follow the evolution of Bragg peaks during magnetic field pulses,^{2,3} i.e., it allows the observations of intensity changes at several scattering angles simultaneously. In our first experiments a MAXIPIX detector¹⁴ was used. This is a fast readout, active pixel detector based on the Medipix2¹⁵ and Timepix¹⁶ readout chips developed by CERN and the Medipix2 collaboration. The system achieves up to 1.4 kHz frame rate with 290 μs minimum readout dead time and has a pixel size of

$55 \times 55 \mu\text{m}^2$. We used the single chip (256×256 pixels) detection geometry. In this geometry, with the detector mounted on the detector arm (γ -arm) of the diffractometer at a distance of 53 cm from the sample, the accessible angular width in both the vertical and horizontal direction is around $\pm 0.8^\circ$, and the angular resolution corresponding to the pixel size is approximately 0.006° in 2θ . The resolution could be increased by increasing the distance to the sample, e.g., to 0.0037° at 85 cm from the sample. This, however, reduces the angular field of view to $\pm 0.5^\circ$ in both the vertical and horizontal direction.

The high frame rate of this detector perfectly matches the time structure of magnetic field pulse and enables multi-frame acquisition as already implemented in other x-ray techniques combined with pulsed fields.¹⁷ Similarly, synchronized with the field pulse, the MAXIPIX detector allows to follow the evolution of Bragg reflections as a function of time during a magnetic field pulse. In our experiments, each frame was exposed during 1.4 ms with a data transfer time of 0.6 ms resulted in an effective frame rate of 500 Hz. In this multi-frame acquisition mode, 50 frames were acquired for each magnetic field pulse, with two frames being recorded before the triggering of the pulse (see Fig. 9).

Raw data obtained are images of the reciprocal space with the scattering angle 2θ along the horizontal direction. For the following, we will call γ the out of diffraction plane angle (vertical direction on raw images) by analogy to the detector arm. To extract the diffracted intensity as a function of time, frames measured in a single magnetic field pulse are first γ -integrated. The resulting 2θ -scans are then concatenated to form an image showing the diffracted intensity at specified scattering angles as a function of time. Typical plots obtained

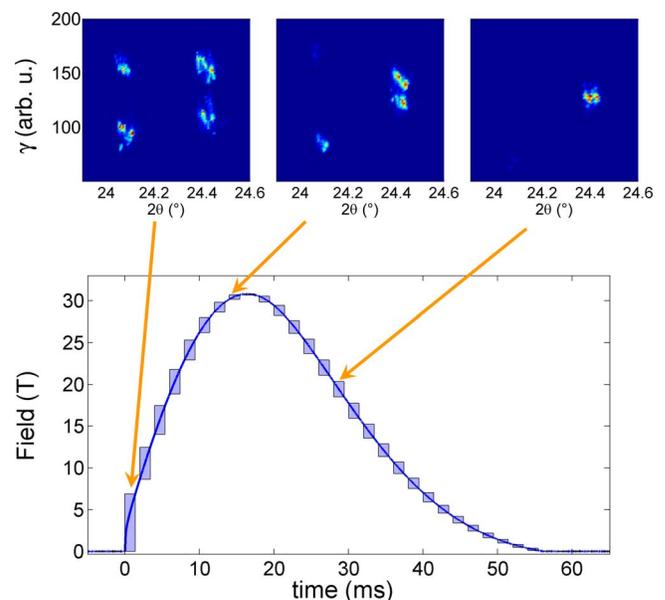


FIG. 9. Data acquisition scheme used combining the split-pair magnet system and a MAXIPIX detector. Line: trace of magnetic field pulse; boxes: acquisition windows. Each frame was recorded every 2 ms, with an exposure time of 1.4 ms and a readout dead time of 0.6 ms. Incident x-ray energy was $E = 31 \text{ keV}$ ($\lambda = 0.3995 \text{ \AA}$). Distance sample-detector $\approx 53 \text{ cm}$. Some selected frames above the pulse trace present the field dependence of the (400)/(040) reflections of a $\text{Fe}_{1.1}\text{Te}$ crystal. The temperature of the sample was $T = 23 \text{ K}$.

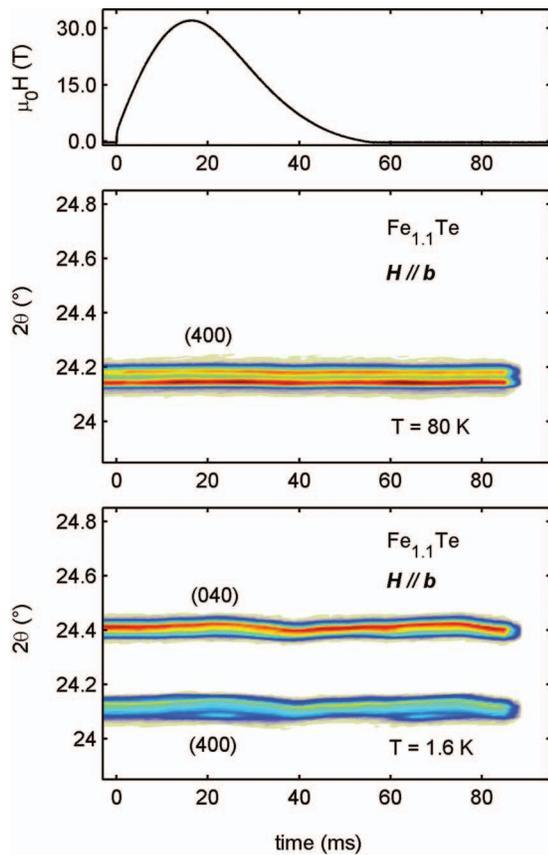


FIG. 10. Time evolution of γ -integrated intensity of the (400) Bragg reflections of $\text{Fe}_{1.1}\text{Te}$ at different temperatures when a magnetic field pulse of 31 T is applied. Below $T_N = 58$ K, the tetragonal (400) splits in the (400)/(040) pair of reflections because of the monoclinic distortion. During the magnetic field pulse (between 0 and 60 ms), there is nearly no evolution of the integrated intensity indicating a quite good sample stability with regard to the beam.

are presented in Figure 10. From these plots, it is then easy to get the intensity variations as a function of field.

B. Example of application: Magnetic-field induced detwinning in $\text{Fe}_{1.1}\text{Te}$

To illustrate the possibilities offered by the combination of our pulsed field set-up with the MAXIPIX detector, first experiments were performed on $\text{Fe}_{1.1}\text{Te}$ single crystals. This compound belongs to the parent phases Fe_{1+x}Te of chalcogenide superconductors $\text{Fe}(\text{Te},\text{Se})$, which are the subject of intense studies because of their similarities and differences with high T_c cuprates. At high temperatures, Fe_{1+x}Te compounds crystallize in the tetragonal $P4/nmm$ structure.¹⁸ Upon cooling the temperature through $T_N \simeq 57\text{--}70$ K,^{18–22} they undergo a first order phase transition leading to an antiferromagnetic (AFM) ordering associated with a structural distortion lowering the high temperature tetragonal paramagnetic lattice symmetry. For $x < 0.12$, the low temperature phase is monoclinic $P2_1/m$ with a bicollinear AFM order whereas it is orthorhombic $Pnmm$ with a strongly incommensurate helimagnetic spin order for $x > 0.12$.^{18,20,21,23} To probe the magneto-elastic couplings which are suspected to play a crucial role in these systems,^{24,25} we performed diffraction experiments on $\text{Fe}_{1.1}\text{Te}$ single crystals over the temperature

range $1.6 < T < 70$ K and in pulsed magnetic fields up to 31 T. The detailed study of this system will be published elsewhere.²⁶ Hereafter, only first results obtained illustrating the possibilities offered by our pulsed field system as regards of field, temperature, and stability are shown.

Single crystals of $\text{Fe}_{1.1}\text{Te}$, grown by a modified Bridgman method, were kindly provided by Viennois and Giannini from Geneva University (Switzerland). A single crystal sample was mounted on the sample holder as described above. The sample was aligned with $[1\ 0\ 0]$ and $[0\ 0\ 1]$ axes in the diffraction plane giving access to Bragg reflections in the $(H, 0, L)$ zone axes. The magnetic field was applied along the b -axis of the crystal. X-ray diffraction images were recorded as described above, using an x-ray photon energy of 31 keV.

We first performed zero field measurements to collect the temperature dependence of several Bragg reflections at different scattering angles. The high temperature tetragonal (400) and (040) Bragg peaks were, for instance, measured. These measurements confirm that our $\text{Fe}_{1.1}\text{Te}$ sample undergoes a structural transition from a tetragonal lattice symmetry at room temperature to a monoclinic one below $T_N \simeq 58$ K, in agreement with previous results.^{21,22,27} The insets in Figure 9 show typical data acquired at $T = 23$ K, below the phase transition. The leftmost image, similar to the frames acquired at $B = 0$ before the field pulse, clearly shows four reflections corresponding to the twinned monoclinic domains that arise at the structural phase transition.²⁵ The peaks are identified as (400) at $2\theta = 24.10^\circ$ and (040) at $2\theta = 24.40^\circ$.

Next, we applied the magnetic field. The evolution at $T = 23$ K of the (400)/(040) Bragg reflections during a 31 T pulse is illustrated, for instance, by the three selected frames shown in Figure 9 (top). At the beginning of the pulse, four Bragg peaks are observed, as described above. Then, during the rise of the field, a progressive disappearance of the low angle Bragg peaks at the benefit of the high angle ones occurs. At 31 T and for all frames measured during the fall of the pulse only one peak remains as shown in the rightmost frame (Fig. 9). This clearly reveals a magneto-crystalline selection of domain leading to the detwinning of the crystal, as already observed in similar systems, applying either high magnetic field^{28–30} or uniaxial pressure.^{31,32}

Figure 10 shows the time dependence of the integrated intensities of the (400)/(040) pair of reflections measured at $T = 80$ K and $T = 1.6$ K when a 31 T magnetic field pulse was applied. Above the Néel temperature (Fig. 10, middle), only one well defined Bragg reflection was observed according with the tetragonal symmetry of the system. No evolution of the integrated intensity was detected as a function of time (and therefore as a function of field), clearly indicating a quite good sample stability with regard to the beam during a 31 T pulse. At $T = 1.6$ K (Fig. 10, bottom), the (400) and (040) reflections are measured simultaneously because of the twinning occurring at the transition, as already observed at 23 K. Upon the application of the magnetic field, only slight oscillations are visible, both peaks keeping their intensity during the whole pulse. This result not only confirms the stability of the measurement, but also indicates that the high field limit of our experimental set-up is not enough to detwin this compound at very low temperature.

In conclusion, this first experiment shows that the vibrations induced by our pulsed field set-up are weak enough to not disturb the measurement when a fast two-dimensional pixel detector is used, thus allowing to follow directly, thanks to the multi-frame acquisition mode, the field dependence of several Bragg reflections during the whole pulse length of 60 ms. This experiment also reveals that applying high magnetic field induces magneto-crystalline domain selection in $\text{Fe}_{1.1}\text{Te}$. These promising results open the door to the investigation of the H - T phase diagram of this material in the limits offered by our experimental set-up.

V. CONCLUSION

In summary, we have constructed a split-pair magnet implemented in a novel cryogenic environment to perform high field single crystal x-ray diffraction measurements at synchrotron sources. This new device offers a panoramic access to x-rays allowing measurements at any scattering angle. It provides magnetic fields up to 31 T with a long pulse duration (rise time of 16.5 ms), which is of great advantage for studying metallic samples, hysteretic effects, and weak signals such as super-lattice peaks. Furthermore, a temperature as low as 1.5 K can be maintained on the sample for more than 10 h using the closed cycle mode of the ^4He cryostat inserted into the bore of the magnet.

During the commissioning of this apparatus, particular attention was given to the problem of field-pulse induced vibrations of the sample. We succeeded to limit the sample rotation induced by magnetic field pulse to $\pm 0.001^\circ$ during the first half of the pulse. This rotation is well below the mosaicity of most single crystal samples of interest for high field studies.

Combined with a fast two-dimensional pixel detector adapted to the time structure of the field pulse, it offers the possibility to follow the intensity changes of several Bragg peaks at different scattering angles simultaneously and throughout the whole duration of the pulse.

Improvements could be carried out on the duty cycle of the experiment by incorporating LN2 cooling channels in the design of the coil. This will decrease the cooling time of the coil but this will come at the expense of the maximal field or will require higher energy.

This device offers the opportunity to investigate small crystallographic changes, such as magneto-elastic effects, field induced symmetry breaking, or charge order that could occur in strongly correlated electrons systems like, e.g., high T_c superconductors, quantum spin systems, or heavy fermions materials.

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